

### CLAIMS

What is claimed is:

1. A method, a sensor array that employs a parameter to induce a time-varying phase angle  $\phi$  on an optical signal that comprises a phase generated carrier with a demodulation phase offset  $\beta$ , the method comprising the steps of:

filtering an output signal from the sensor array to create a filtered signal; and

calculating the phase angle  $\phi$  independently of the demodulation phase offset  $\beta$  through employment of the filtered signal.

2. The method of claim 1, further comprising the step of:

sampling an output signal from the sensor array to obtain a plurality of samples  $S_n$ , wherein  $n = 0$  to  $x$ ;

wherein the step of calculating the phase angle  $\phi$  independently of the demodulation phase offset  $\beta$  through employment of the filtered signal comprises the step of:

calculating the phase angle  $\phi$  independently of the demodulation phase offset  $\beta$

through employment of one or more of the plurality of samples  $S_n$ .

3. The method of claim 1, wherein the step of calculating the phase angle  $\phi$  independently of the demodulation phase offset  $\beta$  through employment of the one or more of the plurality of samples  $S_n$  comprises the steps of:

calculating one or more quadrature terms and one or more in-phase terms through  
5 employment of one or more of the plurality of samples  $S_n$ , wherein one or more of the one or more quadrature terms and one or more of the one or more in-phase terms are substantially independent from the demodulation phase offset  $\beta$ ; and

calculating the phase angle  $\phi$  through employment of the one or more quadrature terms and the one or more in-phase terms.

10 4. The method of claim 2, wherein the output signal comprises a period  $T_{\text{pulse}}$ , wherein the step of sampling the output signal from the sensor array to obtain the plurality of samples  $S_n$ , wherein  $n = 0$  to  $x$  comprises the step of:

sampling the output signal from the sensor array to obtain a plurality of samples  $S_n$  within a period  $T_s$ , wherein  $n = 0$  to  $x$ , wherein  $T_s$  is less than or equal to  $T_{\text{pulse}}$ .

15 5. The method of claim 4, wherein the step of calculating the phase angle  $\phi$  independently of the demodulation phase offset  $\beta$  through employment of the one or more of the plurality of samples  $S_n$  comprises the steps of:

calculating one or more quadrature terms and one or more in-phase terms through  
employment of one or more of the plurality of samples  $S_n$ , wherein one or more of the one or  
20 more quadrature terms and one or more of the one or more in-phase terms are substantially independent from the demodulation phase offset  $\beta$ ;

calculating the phase angle  $\phi$  through employment of the one or more quadrature terms and the one or more in-phase terms.

6. The method of claim 5, wherein the step of calculating the one or more quadrature terms and the one or more in-phase terms through employment of the one or more of the plurality of samples  $S_n$ , wherein the one or more of the one or more quadrature terms and the one or more of the one or more in-phase terms are substantially independent of the

5 demodulation phase offset  $\beta$  comprises the steps of:

calculating a set of quadrature terms  $Q_j$  and a set of in-phase terms  $I_k$  through employment of one or more of the plurality of samples  $S_n$ , wherein  $j = 0$  to  $y$ , wherein  $k = 0$  to  $z$ ;

calculating a quadrature term  $Q_s = \sqrt{\sum_{j=0}^{j=y} Q_j^2}$ , wherein  $Q_s$  is substantially

10 independent of the demodulation phase offset  $\beta$ ;

calculating an in-phase term  $I_s = C_1 \times \sqrt{\sum_{k=0}^{k=z} I_k^2}$ , wherein  $I_s$  is substantially

independent of the demodulation phase offset  $\beta$ ; and

calculating the constant  $C_1$  such that a maximum magnitude of the quadrature term  $Q_s$  and a maximum magnitude of the in-phase term  $I_s$  comprise a substantially same magnitude

15 for a modulation depth  $M$  of an operating range for the phase generated carrier.

7. The method of claim 6, wherein  $x = 7$ ,  $y = 3$ ,  $z = 1$ , wherein the step of calculating the set of quadrature terms  $Q_j$  and the set of in-phase terms  $I_k$  through employment of the one or more of the plurality of samples  $S_n$ , wherein  $j = 0$  to  $y$ , wherein  $k = 0$  to  $z$  comprises the steps of:

5 calculating  $Q_0 = S_0 - S_4$ ;

calculating  $Q_1 = S_1 - S_5$ ;

calculating  $Q_2 = S_2 - S_6$ ;

calculating  $Q_3 = S_3 - S_7$ ;

calculating  $I_0 = (S_0 + S_4) - (S_2 + S_6)$ ; and

10 calculating  $I_1 = (S_1 + S_5) - (S_3 + S_7)$ .

8. The method of claim 6, wherein  $x = 15$ ,  $y = 7$ ,  $z = 3$ , wherein the step of calculating the set of quadrature terms  $Q_j$  and the set of in-phase terms  $I_k$  through employment of the one or more of the plurality of samples  $S_n$ , wherein  $j = 0$  to  $y$ , wherein  $k = 0$  to  $z$  comprises the steps of:

- 5        calculating  $Q_0 = S_0 - S_8$ ;
- calculating  $Q_1 = S_1 - S_9$ ;
- calculating  $Q_2 = S_2 - S_{10}$ ;
- calculating  $Q_3 = S_3 - S_{11}$ ;
- calculating  $Q_4 = S_4 - S_{12}$ ;
- 10       calculating  $Q_5 = S_5 - S_{13}$ ;
- calculating  $Q_6 = S_6 - S_{14}$ ;
- calculating  $Q_7 = S_7 - S_{15}$ ;
- calculating  $I_0 = (S_0 + S_8) - (S_4 + S_{12})$ ;
- calculating  $I_1 = (S_1 + S_9) - (S_5 + S_{13})$ ;
- 15       calculating  $I_0 = (S_2 + S_{10}) - (S_6 + S_{14})$ ; and
- calculating  $I_1 = (S_3 + S_{11}) - (S_7 + S_{15})$ .

9. The method of claim 6, wherein the step of calculating the phase angle  $\varphi$  through employment of the one or more quadrature terms and the one or more in-phase terms comprises the steps of:

calculating a quadrature term  $Q$  from a magnitude of the quadrature term  $Q_s$  and one  
5 or more quadrature terms of the set of quadrature terms  $Q_j$ ;

calculating an in-phase term  $I$  from a magnitude of the in-phase term  $I_s$  and one or  
more in-phase terms of the set of in-phase terms  $I_k$ ; and

calculating the phase angle  $\varphi$  of the output signal from an arctangent of a quantity  $Q /$   
I.

10. An apparatus, a sensor array that employs a parameter to induce a time-varying phase angle  $\phi$  on an optical signal that comprises a phase generated carrier with a demodulation phase offset  $\beta$ , the apparatus comprising:

5 a filter component that filters an output signal from the sensor array to create a filtered signal; and

a processor component that employs the filtered signal to calculate the phase angle  $\phi$  independent from the demodulation phase offset  $\beta$ .

11. The apparatus of claim 10, wherein the processor component obtains a plurality of samples  $S_n$  of the filtered signal, wherein  $n = 0$  to  $x$ ;

10 wherein the processor component employs one or more of the plurality of samples  $S_n$  to calculate the phase angle  $\phi$  independent from the demodulation phase offset  $\beta$ .

12. The apparatus of claim 11, wherein the processor component employs one or more of the plurality of samples  $S_n$  of the output signal to calculate one or more quadrature terms and one or more in-phase terms, wherein one or more of the one or more quadrature terms and one or more of the one or more in-phase terms are substantially independent from  
15 the demodulation phase offset  $\beta$  of the phase generated carrier;

wherein the processor component employs the one or more quadrature terms and the one or more in-phase terms to calculate the phase angle  $\phi$ .

13. The apparatus of claim 11, wherein the output signal comprises a period  $T_{\text{pulse}}$ ,  
20 wherein the processor component obtains the plurality of samples  $S_n$  within a period  $T_s$ , wherein  $T_s$  is less than or equal to  $T_{\text{pulse}}$ .

14. The apparatus of claim 13, wherein the processor component employs one or more of the plurality of samples  $S_n$  of the output signal to calculate one or more quadrature terms and one or more in-phase terms, wherein one or more of the one or more quadrature terms and one or more of the one or more in-phase terms are substantially independent from  
5 the demodulation phase offset  $\beta$  of the phase generated carrier;

wherein the processor component employs the one or more quadrature terms and the one or more in-phase terms to calculate the phase angle  $\phi$ .

15. The apparatus of claim 14, wherein the one or more of the one or more quadrature terms comprise a quadrature term  $Q_s$ , wherein the one or more of the one or more  
10 in-phase terms comprise an in-phase term  $I_s$ ;

wherein the processor component employs one or more of the plurality of samples  $S_n$ , the quadrature term  $Q_s$ , and the in-phase term  $I_s$  to calculate the phase angle  $\phi$ .

16. The apparatus of claim 15, wherein the processor component employs the plurality of samples  $S_n$  to calculate a set of quadrature terms  $Q_j$  and a set of in-phase terms  $I_k$ ,  
15 wherein  $j = 0$  to  $y$ , wherein  $k = 0$  to  $z$ ;

wherein the processor component employs the set of quadrature terms  $Q_j$  and the set of in-phase terms  $I_k$  to calculate the quadrature term  $Q_s$ , and the in-phase term  $I_s$ .



17. The apparatus of claim 16, wherein the processor component calculates a constant  $C_1$ , wherein the processor component calculates:

$$Q_s = \sqrt{\sum_{j=0}^{j=y} Q_j^2};$$

wherein the processor component calculates:

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$$I_s = C_1 \times \sqrt{\sum_{k=0}^{k=z} I_k^2};$$

wherein the processor component calculates the constant  $C_1$  such that a magnitude of the quadrature term  $Q_s$  and a magnitude of the in-phase term  $I_s$  comprise a substantially same magnitude at a modulation depth  $M$  of an operating range for the phase generated carrier.

18. The apparatus of claim 17, wherein the processor component employs the  
10 quadrature term  $Q_s$  and the set of quadrature terms  $Q_j$  to calculate a quadrature term  $Q$ , wherein the processor component employs the in-phase term  $I_s$  and the set of in-phase terms  $I_k$  to calculate an in-phase term  $I$ ;

wherein the processor component calculates:

$$Q = \pm Q_s;$$

15 wherein the processor component calculates:

$$I = \pm I_s;$$

wherein the processor component employs the set of quadrature terms  $Q_j$  to determine a sign of  $Q$ ;

20 wherein the processor component employs the set of in-phase terms  $I_k$  to determine a sign of  $I$ ;

wherein the processor component calculates:

$$\phi = \arctangent (Q / I).$$

19. The apparatus of claim 18, wherein  $x = 7$ ,  $y = 3$ , and  $z = 1$ ;

wherein the processor component calculates:

$$Q_0 = S_0 - S_4, Q_1 = S_1 - S_5, Q_2 = S_2 - S_6, \text{ and } Q_3 = S_3 - S_7;$$

wherein the processor component calculates:

$$I_0 = (S_0 + S_4) - (S_2 + S_6); \text{ and}$$

$$I_1 = (S_1 + S_5) - (S_3 + S_7).$$

20. The apparatus of claim 18, wherein  $x = 15$ ,  $y = 7$ , and  $z = 3$ ;

wherein the processor component calculates:

$$Q_0 = S_0 - S_8, Q_1 = S_1 - S_9, Q_2 = S_2 - S_{10}, Q_3 = S_3 - S_{11},$$

$$Q_4 = S_4 - S_{12}, Q_5 = S_5 - S_{13}, Q_6 = S_6 - S_{14}, \text{ and } Q_7 = S_7 - S_{15};$$

wherein the processor component calculates:

$$I_0 = (S_0 + S_8) - (S_4 + S_{12}), I_1 = (S_1 + S_9) - (S_5 + S_{13}),$$

$$I_2 = (S_2 + S_{10}) - (S_6 + S_{14}), \text{ and } I_3 = (S_3 + S_{11}) - (S_7 + S_{15}).$$

21. The apparatus of claim 10, wherein the period  $T_{pgc}$  of the phase generated  
 15 carrier comprises a frequency  $f_{pgc}$  equal to  $1 / T_{pgc}$ , wherein the frequency  $f_{pgc}$  is  
 approximately between 2 MHz and 20 MHz, wherein the phase generated carrier comprises a  
 modulation depth  $M$  approximately between 1.0 radians and 1.7 radians, wherein the filter  
 component comprises a 3dB roll-off frequency approximately between 10 MHz and 60 MHz.

22. The apparatus of claim 21, wherein the filter component comprises a fourth  
 20 order Bessel low-pass filter.

23. The apparatus of claim 21, wherein the filter component comprises a fourth  
 order real pole filter.

24. An article, a sensor array that employs a parameter to induce a time-varying phase angle  $\phi$  on an optical signal that comprises a phase generated carrier with a demodulation phase offset  $\beta$ , the article comprising:

one or more computer-readable signal-bearing media;

5 means in the one or more media for filtering an output signal from the sensor array to create a filtered signal; and

means in the one or more media for calculating the phase angle  $\phi$  independently of the demodulation phase offset  $\beta$  through employment of the filtered signal.

25. The article of claim 24, further comprising:

10 means in the one or more media for sampling the filtered signal to obtain a plurality of samples  $S_n$ , wherein  $n = 0$  to  $x$ ;

wherein the means in the one or more media for calculating the phase angle  $\phi$  independently of the demodulation phase offset  $\beta$  through employment of the filtered signal comprises:

15 means in the one or more media for calculating the phase angle  $\phi$  independently of the demodulation phase offset  $\beta$  through employment of one or more of the plurality of samples  $S_n$ .

26. The article of claim 25, wherein the means in the one or more media for calculating the phase angle  $\phi$  independently of the demodulation phase offset  $\beta$  through employment of the one or more of the plurality of samples  $S_n$  comprises:

means in the one or more media for calculating one or more quadrature terms and one  
5 or more in-phase terms through employment of one or more of the plurality of samples  $S_n$ ,  
wherein one or more of the one or more quadrature terms and one or more of the one or more  
in-phase terms are substantially independent from the demodulation phase offset  $\beta$ ; and

means in the one or more media for calculating the phase angle  $\phi$  through  
employment of the one or more quadrature terms and the one or more in-phase terms.

10 27. The article of claim 26, wherein the output signal comprises a period  $T_{\text{pulse}}$ ,  
wherein the means in the one or more media for sampling the output signal from the sensor  
array to obtain the plurality of samples  $S_n$ , wherein  $n = 0$  to  $x$  comprises:

means in the one or more media for sampling the output signal from the sensor array  
to obtain the plurality of samples  $S_n$  within a period  $T_s$ , wherein  $n = 0$  to  $x$ , wherein  $T_s$  is less  
15 than or equal to  $T_{\text{pulse}}$ .

28. The article of claim 27, wherein the means in the one or more media for calculating the phase angle  $\phi$  independently of the demodulation phase offset  $\beta$  through employment of the one or more of the plurality of samples  $S_n$  comprises:

means in the one or more media for calculating one or more quadrature terms and one  
5 or more in-phase terms through employment of one or more of the plurality of samples  $S_n$ ,  
wherein one or more of the one or more quadrature terms and one or more of the one or more  
in-phase terms are substantially independent from the demodulation phase offset  $\beta$ ; and

means in the one or more media for calculating the phase angle  $\phi$  through  
employment of the one or more quadrature terms and the one or more in-phase terms.

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